

# Information acquisition system of multipoint soil surface height variation for profiling mechanism of seeding unit of precision corn planter

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**Abstract:** The emergence rate and vitality of maize are directly affected by the sowing depth, and the uniformity of this depth is an important performance indicator of a planter, while the effective soil surface height information acquisition is the prerequisite for ensuring the accuracy of sowing depth control. The soil surface height variation acquisition system of a precision corn planter often produces profiling errors when performing active profiling due to interference from ground debris. In this study, a multipoint soil surface height variation information acquisition system was investigated, which consists of a ranging sensor group and a microcontroller unit (MCU) using a data comparison and screening method. The structure and specifications of the ranging sensors were determined according to the soil surface height variation and debris size, and a nonessential profiling control program was developed. Performed tests on the information acquisition system indicated that the measurement accuracy of the system was 3 mm, and when advancing at a speed of 8 km/h, the accuracy of the profiling decision and the system stability were 97.1% and 94.1%, respectively, indicating that the system was capable of nonessential profile control. The designed ranging system could provide a reference for the design of a ground information acquisition system of precision planters with an active profiling mechanism.

**Keywords:** corn, precision planter, information acquisition system, seeding unit, profiling mechanism, active profiling, soil surface height variation

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## 1 Introduction

The emergence rate and the growth of seedlings are affected by the sowing depth<sup>[1-3]</sup>; a reasonable and uniform sowing depth can improve the plant emergence rate, seedling quality and plant vitality in later growing stages, which is conducive to crop production<sup>[4]</sup>. The furrow depth for sowing operations is one of the main factors affecting the sowing depth<sup>[5]</sup>. Profiling mechanisms with satisfactory performance enable the furrow opener of a planter to maintain a stable working depth while accommodating terrain changes and are thus important in controlling the furrowing depth<sup>[6-8]</sup>. Two types of adjustments, namely, passive adjustment and active adjustment, have been adopted to control the furrowing depth by the profiling mechanism of the seeding unit<sup>[9]</sup>, of which the passive adjustment shows poor adaptability due to the interference of the seeding unit weight and

the ground support force, while the active adjustment provides better ground adaptability because the profiling mechanism itself provides the furrow depth control power<sup>[10]</sup>. The accuracy of the surface height variation information acquired by active profiling mechanism directly affects the furrowing accuracy and uniformity<sup>[11]</sup>; thus, accurately obtaining such information is one of the key aspects in designing an efficient active profiling mechanism<sup>[12]</sup>.

Characterization of the soil surface height variation has been achieved through both contact and noncontact measurements<sup>[13-15]</sup>. At present, the contact measurement system is the predominant method used in China. In the past, to measure the soil surface height variation, a profiling pallet or ground rolling wheel were used as the grounding part, and an electronic ruler, angle sensor and switch sensor were used to acquire translation and rotation signals from the grounding part<sup>[16-21]</sup>. Mouazen et al.<sup>[22]</sup> and Saeys et al.<sup>[23]</sup> measured the soil surface height variation by acquiring the impact of surface height variations on the sensor through a ground-contact pressure sensor; Jensen et al.<sup>[24]</sup> mounted the sensor on the depth control wheel and measured the height variation through sensing the coincidence of the depth control wheel; Subsequently, Anthonis et al.<sup>[25]</sup> found that the accuracy of this method was affected by the soil surface compactness. Zhao et al.<sup>[26]</sup> mounted a PVDF strain sensor to the inner surface of the wheel so that the output voltage of the sensor was determined by the wheel strain and established a voltage signal and strain relationship model to detect soil surface height variation. Zielke<sup>[27]</sup> developed a mobile real-time soil humidity detection sensor to control the sowing depth based on the appropriate soil moisture, which is now in the promotion stage. Wen et al.<sup>[28]</sup>

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found that the contact measurement method is straightforward and robust against interference by the external environment but that the inertia generated in the grounding component by the vertical movement of the planter during the high-speed sowing operation leads to inertial errors; such errors affect the measurement result and degrade the accuracy of the grounding part due to excessive wear from extended use. In contrast, the noncontact measurement method can effectively avoid measurement error caused by wear and mechanical inertia<sup>[29]</sup>. With the development of modern agricultural technology, conservation tillage has emerged<sup>[30]</sup>. In the region of Heilongjiang Province, 30% of the corn stalks are shredded and returned to field under conservation tillage practices<sup>[31]</sup>; consequently, after tillage, a large quantity of incompletely shredded corn stalk residuals remain on the ground, interfering with the sensor and causing the system to misclassify debris as a rising surface when acquiring soil surface height variation information, which results in errors in the profiling control of the active profiling mechanism.

To address the issue that the accuracy of single-point soil surface height variation information acquisition is susceptible to debris interference, we have designed a microcontroller unit (MCU)-based noncontact measurement system to acquire high-precision soil surface height variation information while reducing profiling errors under the no-tillage practices. The system thus provides a solution for the acquisition of soil surface height variation information for planters and other ground-height-dependent mechanisms.

## 2 Materials and methods

### 2.1 System structure and working principle

#### 2.1.1 System structure and technical parameters

The structural diagram of the soil surface height variation information acquisition system is shown in Figure 1. The system consists of the measurement hardware, the MCU, and the mechanical structure of the acquisition system. The microcontroller circuit system contains five input ports with A/D conversion connected to the ranging sensor, which converts the analog signal transmitted from the sensor into a digital signal in real time, one data input port to read in microcontroller data, and two D/A output ports with relay switches to output the control signal, as shown in Figure 2. The installation structure of the soil surface height variation information acquisition system, which is schematized in Figure 3, contains the ranging sensor group and the sensor mounting assembly. The main technical parameters of the system are as follows: response time: 0.03 s; height measurement range: 20-500 mm; and accuracy within the measurement range:  $\pm 1$  mm.

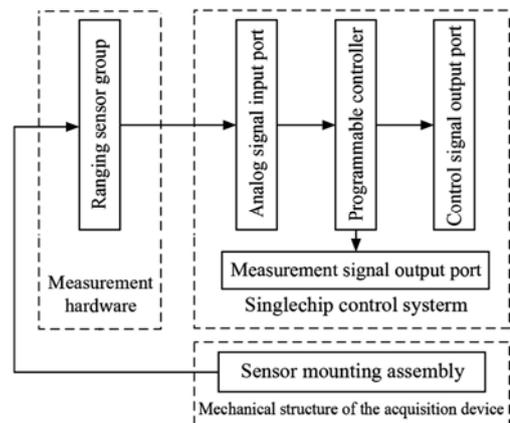


Figure 1 Height information acquisition device structure block diagram

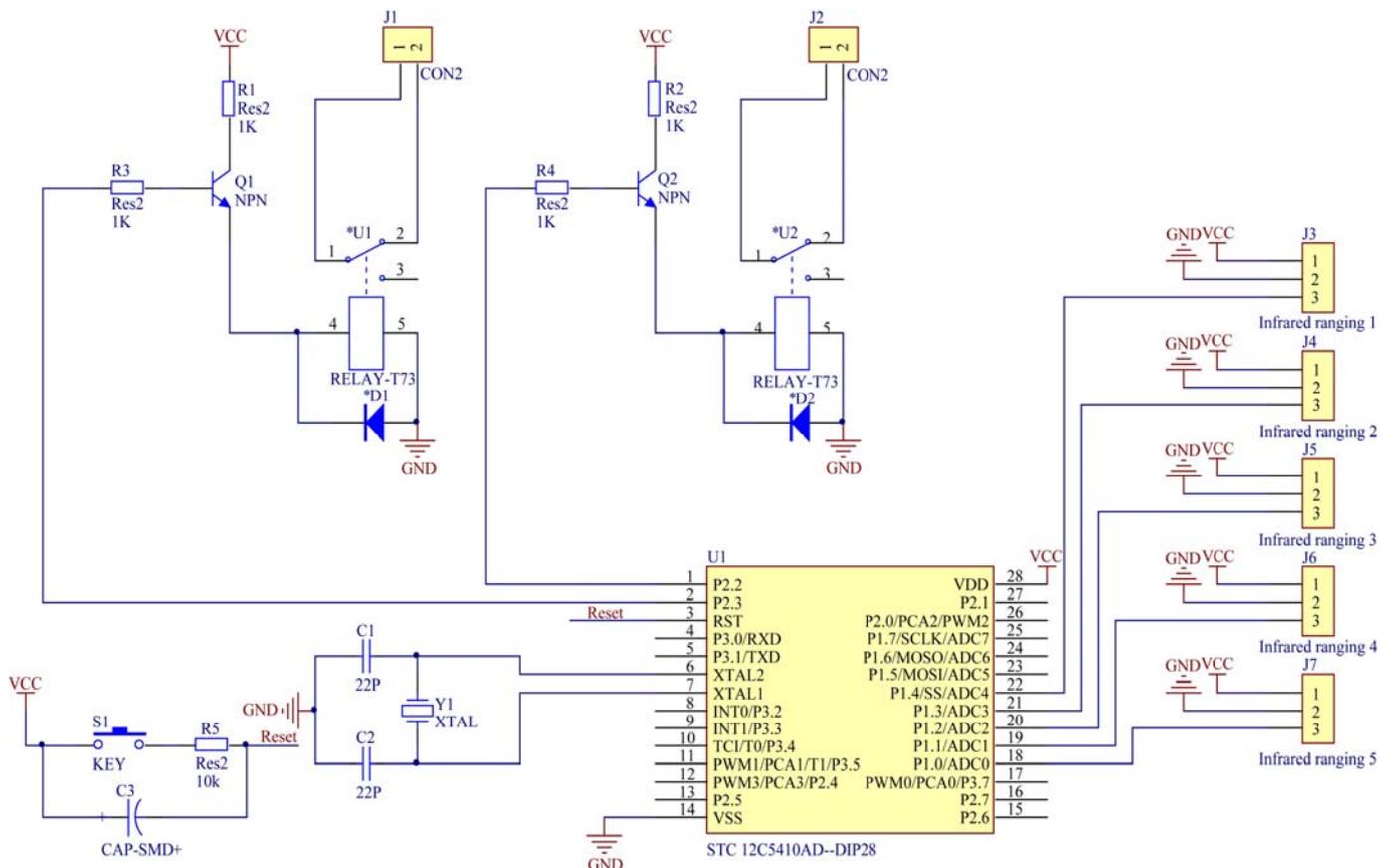
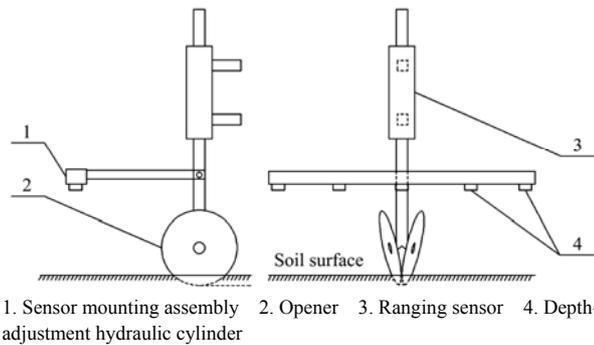


Figure 2 Surface altitude information acquisition system circuit diagram



1. Sensor mounting assembly 2. Opener 3. Ranging sensor 4. Depth-adjustment hydraulic cylinder

Figure 3 Simplified diagram of the installation structure of the highly variable acquisition device

### 2.1.2 Working principle

Before running the system, the initial position of the ranging sensor relative to the soil surface height is set on the MCU, and when measuring, the soil surface height variation measurement mechanism fluctuates vertically with the changing surface topography and provides a baseline for furrowing depth; when the distance change acquired by the sensor directly in front of the opener exceeds the reasonable range, the MCU compares the numerical information collected by the main sensor with the information collected by the other auxiliary sensors and finds the cause of the change in the ranging distance detected by the sensor directly in front of the opener through a difference analysis. When the change is caused by the surface height variation, the MCU operates in response to the change and exports a profiling control signal; otherwise, the change is deemed invalid, and profiling control is not performed.

## 2.2 Design of key components

### 2.2.1 Sensor selection

The methods for noncontact active ranging include laser, radar, ultrasonic, infrared light, and continuous wave radar<sup>[32-44]</sup>. Relative to ultrasonic waves, infrared waves transmit faster with better transmission directivity, higher transmission power controllability, and greater robustness against interference<sup>[45-50]</sup>. Therefore, an infrared ranging sensor was chosen in this study to measure the distance using the triangulation method (Figure 4)<sup>[51]</sup>. The principle of infrared ranging is that an infrared transmitter transmits an infrared beam in a certain angle and that the beam returns when encountering an object; the reflected light is collected by the CCD detector with a shift value, through which, together with the known emission angle  $\alpha$ , the central distance ( $X$ ), and the filter focal length  $f$ , the distance between the sensor and the object ( $D$ ) can be calculated through the triangle geometry. Because of the principle of triangulation, the scanning range of the sensor measurement is not a plane but a point, so an array of sensors is needed to work in concert to achieve the goal of accessing ground interval changes.

### 2.2.2 Determination of the sensor position and quantity

Following tillage, the maximum diameter of the clod is smaller than 50 mm<sup>[52]</sup>. When the conservation tillage is practiced, corn stalks are shredded and returned to the field; the average length of the corn stalk shreds is 52 mm, while the incompletely shredded corn stalks are 100-250 mm in length<sup>[53]</sup>. When acquiring the surface distance information, the presence of clods or corn stalks in the ranging area of the sensor may cause inconsistencies between the surface height variation information and the actual situation, resulting in profiling control errors. By adopting the real-time multi-sensor data comparison method, we can mitigate the interference of debris on soil surface contour information acquisition and thus reduce such errors.

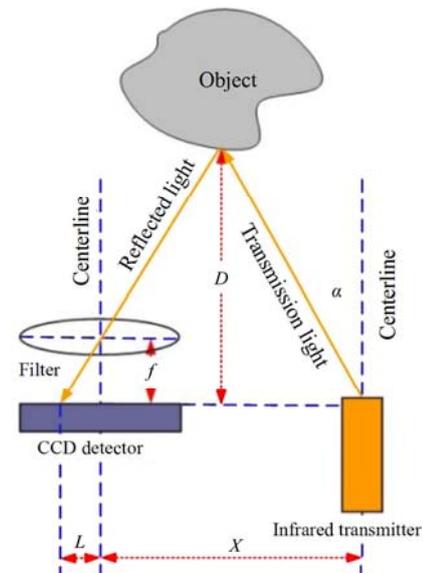
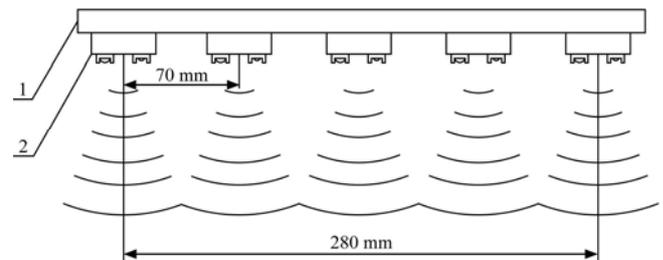


Figure 4 Principle of triangular distance measurement

To accommodate the presence of incompletely shredded stalk pieces in the ranging areas of all the sensors and to avoid the possibility that the actual soil surface height variation information is not acquired by any sensor, the spacing between the sensor should be larger than the diameter of the incompletely tilled clods, and the maximal ranging area of the soil surface height variation information acquisition component should be larger than the maximal length of the incompletely shredded corn stalk (250 mm). Consequently, five infrared ranging sensors are used in the acquisition assembly perpendicular to the moving direction of the planter, with a spacing of 70 mm between the sensors and a ranging width of 280 mm (Figures 5 and 6); the sensor in the center shares the same longitudinal trajectory as the opener.



1. Electronic mounting board 2. Infrared ranging sensor

Figure 5 Locations of the infrared distance sensors



Figure 6 Infrared ranging sensor group

### 2.2.3 Nonessential profiling control principle

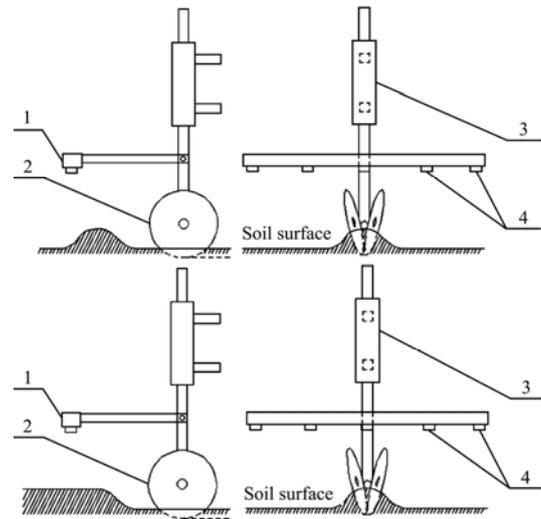
By comparing the 5-point soil surface height variation information transmitted by the ranging sensor component in real time, we analyzed the causes of the change of the sensor measurement data and distinguished the actual surface height

variation from that derived from debris interference to make the profiling decision. In this way, the interference of the ground debris on the ranging sensor is mitigated, the nonessential profiling avoided, and the accuracy of the profiling improved.

In the nonessential profiling control program, the infrared ranging sensor directly in front of the opener is set as the main sensor. When the main sensor detects a distance change, the MCU compares the main sensor signal with the instantaneous signal of each of the four adjacent sensors to determine whether to profile, and if it is necessary to profile, then the profiling is performed with the profiling control according to the soil surface height variation data acquired by the main sensor. The possible scenarios of the surface height variation detected by the main sensor are analyzed to determine the necessary profiling control scheme.

In different ground conditions, the surface height variation information collected by each sensor varies, and the profiling decisions are also different. 1) The system selects profiling control when the field surface is uniformly level, the soil surface height variation is uniform, and the difference between the change in the soil surface height variation acquired by the main sensor and that of each of the remaining four sensors is lower than 5 mm. 2) The system selects profiling control when the sowing field is the furrowed land after the tillage, in which the height at each ranging point within the ranging width varies, the changes sensed by the sensors while advancing are consistent, and the distance information acquired by the main sensor is continuous, with values fluctuating within a reasonable excursion of  $\leq 5$  mm. 3) In cases of small bumps and depressions of soil surface height, clods, or exposed or partially exposed corn stalks, if the main sensor senses the height variation while the auxiliary sensors sense only slight or no variation, the system decides against performing profiling control. 4) If the field is unlevelled, and the heights measured by the five sensors are different, the system makes the decision on profiling control based on the duration of the continuously changing signals acquired by the main sensor. When the opener encounters an extended bump or depression, i.e., the duration of the height changing signal is  $\geq 0.1$  s, the system makes the decision of performing profiling control; otherwise, the system decides against profiling control.

As shown in Figure 7, the signal change information acquired by the sensor group when the opener is aligned with the furrow after tillage is similar to that acquired in the cases of small bumps and depressions of soil surface height, clods, and exposed or partially exposed corn stalks; the difference is that the former is continuous. To distinguish the two ground conditions, the timing of the information acquisition of the main sensor is performed, in which the timing on the signal from the main sensor is started when the soil surface height variation information is acquired by the main sensor and its difference from that of each of the other four sensors is greater than a reasonable value; when the duration is longer than the set time, profiling control is performed, otherwise, profiling control is not performed. The speed of the corn seeding operation is generally 5-8 km/h, and the planting spacing is 20-25 cm, so the average time interval between sowing two seeds is 0.4 s, and the timing duration of 0.1 s is set (during which the planter advances a distance of 139-222 mm). Based on the characteristics of change in the signal acquired by each of the sensors at different soil surface height variations, the profiling control program is designed, as shown in Figure 8.



1. Sensor mounting assembly 2. Opener 3. Ranging sensor 4. Depth-adjustment hydraulic cylinder

Figure 7 Surface small soil bags and ribbon deployment

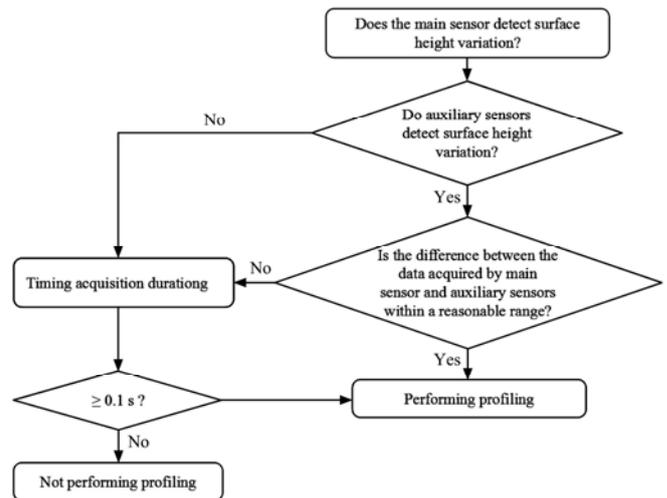


Figure 8 Surface small soil bags and ribbon deployment

2.3 Experiment methods

2.3.1 Test equipment

The nonessential profiling control tests were performed on the soil surface height information acquiring platform (the platform moved along the rail of the soil bin through wheels to ensure the constant level of the sensor group during the test, and the distance between the ranging sensor group and the ground was 350 mm), which was connected to the soil bin test vehicle that was used to supply the pulling force, as shown in Figure 9.



Figure 9 Ground information acquisition test bed and earth tank testing vehicle

2.3.2 Preparations before the test

Before the test, the soil in the soil bin was leveled, and various levels of raised and lowered surfaces (No. 1-6), bumps and potholes (No. 7-10), and furrow areas (No. 11-12) were incorporated in addition to debris sites with clods and incompletely shredded corn stalks (soil measurement sites: No. 13-16; stalk measurement sites: No. 17-26). The metal modules of proximity sensors were mounted on the side of the rail parallel to the test sites for positioning; the soil bin test platform is shown in Figure 10.



Figure 10 Earth slot detection zone

2.3.3 Test content

In the static state, the decision-making ability of the soil surface height variation information acquisition system was tested in the presence of potholes, bumps, clods, and corn stalk pieces

when profiling control is not needed. At the upper speed limit of the corn sowing operation (8 km/h), the furrow area measurement accuracy and the profiling control decision-making accuracy were examined.

3 Results and discussion

3.1 Nonessential profiling control test and results

The designed multipoint surface height variation information acquisition system was tested, and the feasibility, accuracy and stability of the nonessential profiling control of the system were evaluated through static and dynamic tests.

3.2 Test results and analysis

3.2.1 Analysis of results of static measurement test

Sites 1-12 were tested in the static measurement; the soil surface height variation data and the measurement data of five tests are shown in Table 1. The errors of the five measurements were plotted on a line chart, as shown in Figure 11. The mean error of the static measurements was 1.67 mm, the standard deviation of the errors ( $\sigma$ ) of the overall static measurement data (calculated using Equation (1)) was 1.80, and the stability of the system was 94.5%, indicating that the measurement accuracy met the system design requirements.

$$\sigma = \sqrt{\frac{1}{N} \sum_{i=1}^N (x_i - \mu)^2} \tag{1}$$

In the static measurements, the standard error ( $\sigma$ ) of the overall soil surface height variation measurement data was 1.84, and the stability of the system was 93.9%; the standard error ( $\sigma$ ) of the soil surface height variation data of the individual site and the furrow area was 2.13, and the stability of the system was 95.1%.

Table 1 Static measurement data

Type of change		Soil surface height variation/mm					Type of change		Soil surface height variation at the individual site and furrow area/mm				
No.	Parameter	Test 1	Test 2	Test 3	Test 4	Test 5	No.	Parameter	Test 1	Test 2	Test 3	Test 4	Test 5
1	10	10	9	9	12	10	7	-30×100	-29	-28	-31	-30	-27
2	50	47	48	47	50	49	8	-50×100	-47	-48	-49	-48	-45
3	80	80	79	77	81	77	9	50×130	49	48	52	53	48
4	-10	-9	-7	-9	-8	-10	10	70×160	69	68	69	67	72
5	-50	-48	-49	-49	-50	-47	11	70 ridge	69	68	71	67	69
6	-80	-79	-78	-77	-78	-78	12	-50 trench	-47	-49	-48	-48	-52

3.2.2 Analysis of the dynamic measurement test results

The dynamic measurements were performed on Sites 1-26, of which Sites 13-26 were sites to evaluate the decision making associated with profiling control. The measurements were performed at each site at a moving speed of 8 km/h (Table 2), and the errors of the set soil surface height variation data and the measurement data from five tests were plotted on a line chart, as shown in Figure 12. The measurements in the dynamic tests were similar to those in the static tests; the mean error of the measurements in the furrow area was 2.3 mm, the standard deviation  $\sigma$  of the dynamic measurement data was 2.77, and the stability of the system was 92.1%. In the dynamic measurements, the standard deviation of the error ( $\sigma$ ) of overall soil surface height variation measurement data was 2.63, and the stability of the system was 93.1%; the standard error ( $\sigma$ ) of the soil surface height variation data of the individual site and the furrow area was 2.93, and the stability of the system was 91.8%. Sites 13-26 were the sites with debris, with an expected output value of 0 mm, and

deviation from this value indicates a decision error associated with the profiling control. The nonessential profiling control data are shown in Table 3, and the results show that the accuracy of the nonessential profiling control program was 97.1% and the stability of the system was 94.1%.

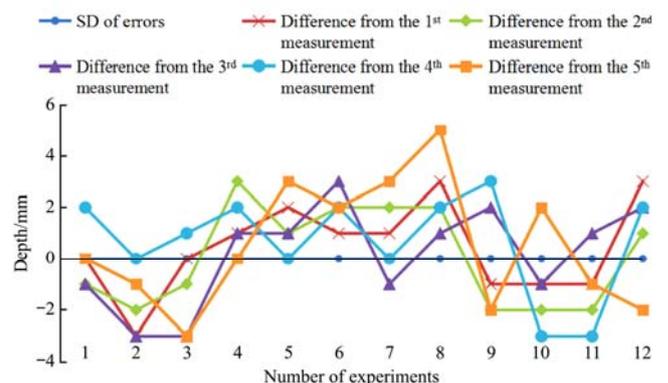


Figure 11 Static measurement error

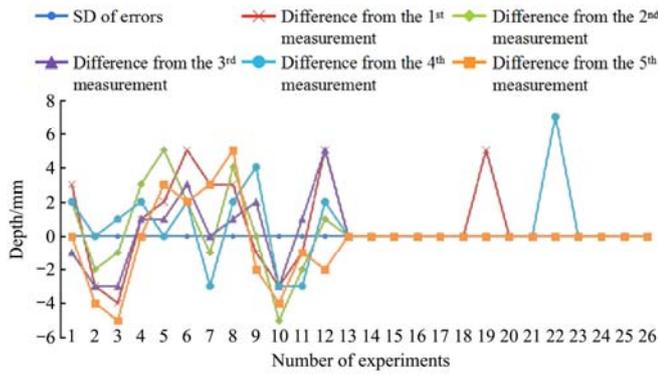


Figure 12 Dynamic measurement

Based on the above analyses, the soil surface height variation information acquisition system was tested through static and dynamic measurements; the experimental methods and the system response time (0.03 s) were identical to those of Wen et al.<sup>[20]</sup> but

with a higher measurement accuracy. In this study, the multipoint active detection method was adopted to acquire the soil surface height variation information, and the profiling decision was made after calculation and screening on multiple soil surface height variation signals using the profiling program; relative to controlling the sowing depth based on a single soil surface height variation signal obtained through single-point measurement<sup>[10]</sup>, the method proposed in this study effectively improved the accuracy of sowing depth control decisions and reduced the incidence of profiling errors. Relative to traditional mechanical and contact ground detection<sup>[12,13,16]</sup>, the proposed method simplified the structure while avoiding mechanical wear. The field experiments showed that in actual field operations, particularly when exposing the sensors to direct high-intensity sunlight, the sensors were occasionally interfered by the sunlight, so small visors were designed and installed near the sensor group to avoid direct sunlight.

Table 2 Dynamic measurement data

Type of change		Soil surface height variation/mm					Type of change		Soil surface height variation at the individual site and furrow area/mm				
No.	Parameter	Test 1	Test 2	Test 3	Test 4	Test 5	No.	Parameter	Test 1	Test 2	Test 3	Test 4	Test 5
1	10	10	8	9	12	10	7	-3000	-29	-28	-31	-30	-30
2	50	47	48	49	50	49	8	-5000	-47	-48	-49	-48	-45
3	80	80	79	77	81	77	9	50×130	49	48	52	53	48
4	-10	-9	-7	-9	-8	-10	10	70×160	69	68	69	67	71
5	-50	-48	-49	-49	-50	-47	11	70 ridge	69	68	71	67	69
6	-80	-79	-78	-77	-78	-78	12	-50 trench	-47	-49	-48	-48	-52

Table 3 Nonessential profiling control data

Debris type		Clods/mm						Corn stalk/mm							
No.	Parameter	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Test groups	1	0	0	0	0	0	0	5	0	0	0	0	0	0	0
	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	4	0	0	0	0	0	0	0	0	0	7	0	0	0	0
	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0

4 Conclusions

In this study, we designed a multipoint surface height variation information acquisition system for the profiling mechanism of the seeding unit of a corn planter; the response time and height measurement range of the system were 0.03 s and 20-500 mm, respectively. The system provides nonessential profiling control, reduces the incidence of profiling error due to the interference of ground debris on the system, and provides a reference for the design of a surface height variation information acquisition system.

1) The measurement accuracy of the surface height variation information acquisition system was 3 mm. The standard error  $\sigma$  of the overall soil surface height variation measurement data was 2.63, and the stability of the system was 93.1%. The standard deviation  $\sigma$  of the errors of surface height variation of the individual site and furrow area was 2.93, and the stability of the system was 91.8%.

2) When acquiring the soil surface height information at a moving speed of 8 km/h, the accuracy of the nonessential profiling

control program was 97.1%, and the stability of the system was 94.1%.

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